

FA42 300



| | | | | | | | $(n_1) = 1400$ -1 | | | | | | | | | | |
|-----------------------|--------------|-----------------|-----------------|------|-----------------|-----------------|-------------------|----|----|----|-----|----|----|------------|------|-----|--|
| n_2 [s^{-1}] | i | P_{1M} [] | M_{2M} [] | f.s. | P_{1R} [] | M_{2R} [] | B5 | | | | B14 | | | | | | |
| | | | | | | | B | C | D | E | Q | R | T | U | | | |
| | | | | | | | 63 | 71 | 80 | 90 | 71 | 80 | 90 | 100 112 | | | |
| 167 | 8,38 | 4 | 215 | 1,0 | 4,0 | 220 | B | | | | C | C | | | 2821 | | |
| 139 | 10,04 | 3 | 194 | 1,1 | 3,4 | 220 | B | | | | C | C | | | 2818 | | |
| 114 | 12,33 | 3 | 238 | 1,0 | 3,0 | 240 | B | | | | C | C | | | 2813 | | |
| 92 | 15,16 | 2,2 | 216 | 1,1 | 2,4 | 240 | B | | | | C | C | | | 1921 | | |
| 80 | 17,57 | 2,2 | 250 | 1,0 | 2,2 | 250 | B | | | | C | C | | | 1721 | | |
| 77 | 18,16 | 2,2 | 258 | 1,0 | 2,3 | 270 | B | | | | C | C | | | 1918 | | |
| 67 | 21,05 | 2,2 | 299 | 1,0 | 2,2 | 300 | B | | | | C | C | | | 1718 | | |
| 63 | 22,30 | 2,2 | 317 | 0,9 | 2,1 | 300 | B | | | | C | C | | | 1913 | | |
| 57 | 24,70 | 1,5 | 242 | 1,2 | 1,9 | 300 | B | | | | C | C | | | 1518 | .30 | |
| 54 | 25,85 | 1,5 | 253 | 1,2 | 1,8 | 300 | B | | | | C | C | | | 1713 | | |
| 47,5 | 29,49 | 1,5 | 289 | 1,0 | 1,6 | 300 | B | | | | C | C | | | 1318 | | |
| 46,1 | 30,34 | 1,5 | 297 | 1,0 | 1,5 | 300 | B | | | | C | C | | | 1513 | .35 | |
| 41,7 | 33,60 | 1,1 | 240 | 1,0 | 1,1 | 250 | B | | | | C | C | | | 1021 | | |
| 38,7 | 36,21 | 1,1 | 259 | 1,2 | 1,3 | 300 | B | | | | C | C | | | 1313 | | |
| 34,8 | 40,25 | 1,1 | 288 | 1,0 | 1,1 | 300 | B | | | | C | C | | | 1018 | | |
| 28,3 | 49,43 | 0,75 | 243 | 1,2 | 0,93 | 300 | B | | | | C | C | | | 1013 | | |
| 26,7 | 52,53 | 0,75 | 258 | 1,0 | 0,73 | 250 | B | | | | C | C | | | 918 | | |
| 21,7 | 64,51 | 0,55 | 234 | 1,3 | 0,71 | 300 | B | | | | C | C | | | 913 | | |
| 20,2 | 69,37 | 0,37 | 168 | 1,1 | 0,40 | 180 | B | | | | C | C | | | 718 | | |
| 16,4 | 85,19 | 0,37 | 206 | 1,1 | 0,39 | 220 | B | | | | C | C | | | 713 | | |

- 0,96.



B)



C)

FA42

1.

2.

| H1 | H4 | H3 | H2 | H5 | H6 |
|---------------------|-------|-------|-----------------------|-------|-------|
| | | | | | |
| -- LT | -- LT | -- LT | -- LT | -- LT | -- LT |
| AGIP Telium VSF 320 | | | SHELL Omala S4 WE 320 | | |

1

$F_{eq} = F_R \cdot \frac{127,5}{X + 97,5}$

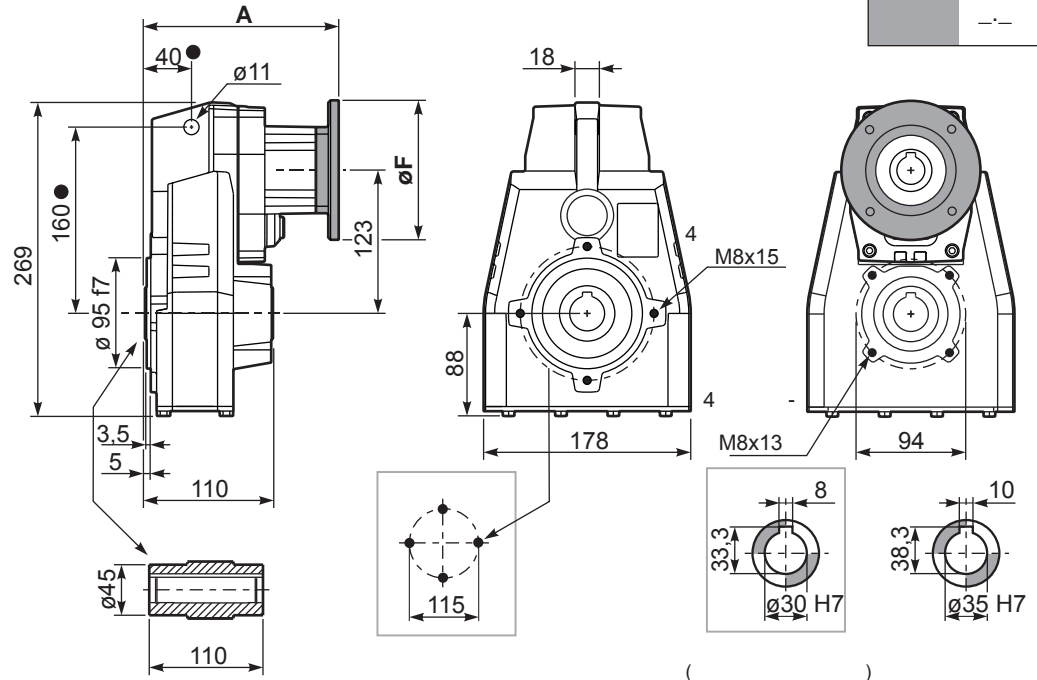
| n_2 [s^{-1}] | FA | FR | n_2 [s^{-1}] | FA | FR | n_2 [s^{-1}] | FA | FR |
|-----------------------|-----|------|-----------------------|-----|------|-----------------------|-----|------|
| 300 | 300 | 1500 | 140 | 390 | 1950 | 70 | 490 | 2450 |
| 250 | 320 | 1600 | 120 | 410 | 2050 | 40 | 590 | 2950 |
| 200 | 350 | 1750 | 85 | 460 | 2300 | 15 | 800 | 4000 |

| n_1 | FA | FR |
|-------|-----|------|
| 1400 | 240 | 1200 |
| 900 | 280 | 1400 |
| 500 | 340 | 1700 |

2

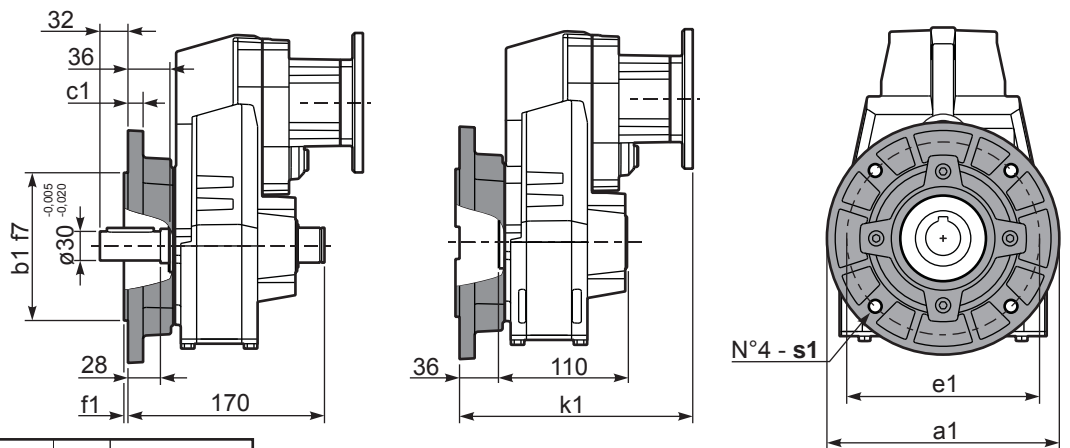
PFA42C...

| | | øF | A |
|------------|------------|-----|-------|
| 63B5 | K063.4.041 | 140 | 169,5 |
| 71B5 | K063.4.042 | 160 | 167,5 |
| 80/90B5 | K063.4.043 | 200 | 169,5 |
| 71B14 | K063.4.047 | 105 | 167,5 |
| 80B14 | K063.4.046 | 120 | 168,5 |
| 90B14 | K063.4.041 | 140 | 169,5 |
| 100/112B14 | KC40.4.041 | 160 | 185 |



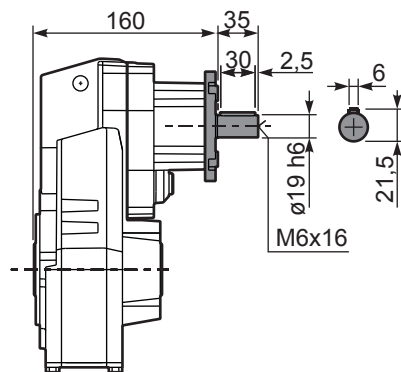
PFA42...-F...

| | k1 |
|------------|-------|
| 63B5 | 205,5 |
| 71B5 | 203,5 |
| 80/90B5 | 205,5 |
| 71B14 | 203,5 |
| 80B14 | 204,5 |
| 90B14 | 205,5 |
| 100/112B14 | 221 |

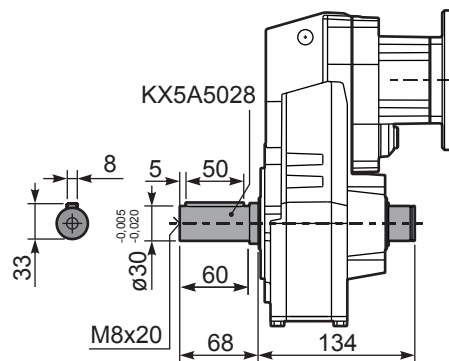


| a1 ø | b1 | c1 | e1 | f1 | s1 | |
|------|-----|----|-----|-----|----|------------|
| 160 | 110 | 10 | 130 | 3 | 9 | KX5A.9.010 |
| 200 | 130 | 13 | 165 | 3.5 | 11 | KX5A.9.011 |
| 250 | 180 | 14 | 215 | 4 | 14 | KX5A.9.012 |

RFA42C...



PFA42 A...



PFA42D...

